

Adjustment arrangement of an optical element

The invention relates to an adjustment arrangement of an optical element, in particular of a lens in an optical system. The invention also relates to a projection lens system in semiconductor lithography with a number of optical elements and with at least one adjustment arrangement for an optical element.

EP 1 014 139 A2 discloses an optical system for comparable purposes, in which an optical element, in particular a lens, is mounted on a multiplicity of angular bearing feet arranged in a uniformly distributed manner over the circumference of an inner ring or a mount. These bearing feet have the effect of providing on the one hand precise mounting and on the other hand appropriate elasticity for introducing deformations onto the lens as the optical element. The deformations are in this case applied to an inner ring of a mount that is connected to all the bearing feet and are transferred through the bearing feet to the region of the optical element.

However, it is a disadvantage of this arrangement that the specific deformation of the optical element is made more difficult by the distortions of the inner ring, which cannot be sufficiently predicted in each case, influencing the deformations that are to be transferred to the lens. The deformations of the inner ring are passed on to the optical element via a certain number of the bearing feet that are present. To distort the optical element in a specific way, it would have to be known exactly how the inner ring reacts to the respective distortions and how the latter are transferred to

the optical element from the region of the inner ring and by which of the bearing feet.

Since, however, these effects cannot be calculated with
5 the required accuracy and cannot be reproducibly repeated, this represents a disadvantage of such a construction, since the specific, punctiform transfer of deformations to the optical element is adversely affected by the construction in a way which cannot be re-
10 produced.

For further prior art, reference is made to US 4,993,823, WO 99/67683, US 6,552,862 B2 and US 6,580,570.

15 Incorporated by reference are US 6,307,688, US 10/002,097 and US 10/661,183.

It is therefore the object of the present invention to
20 provide a arrangement for the passive and active adjustment of an optical element which, apart from the required precise mounting and the simultaneously desired elasticity of the mounting, also allows the selective introduction of deformations into the region of
25 the optical element.

This object is achieved according to the invention in the case of an adjustment arrangement of an optical element, in particular of a lens in an optical system,
30 the optical element having a circumference and being mounted in a mount by a number of bearing feet arranged in a distributed manner over the circumference of the optical element, the optical element being selectively

deformable by actuators, and at least some of the bearing feet being engaged by at least one actuator in such a way that the respective bearing foot can be displaced in a direction substantially orthogonal to said circumference.

The fact that the actuators engage in the region of the respective bearing foot in such a way that they displace the bearing foot itself, and consequently deform the optical element, allows very specific introduction of the desired deformations into the optical element to be achieved without this process being affected by the often unreproducible effects which could occur, for example, in the case of deformation of an inner ring of the mount.

It is for instance possible in a particularly advantageous way to achieve a deformation of the optical element by means of a force, without thereby changing the position of said element, by introducing the forces into the bearing feet. This is made possible by the pinpoint engagement in the region of the bearing feet, so that deformation and manipulation can be adjusted or regulated in relation to one another in such a way that they can be monitored.

In a particularly favorable development of the invention, the number of bearing feet is in this case significantly reduced in comparison with the prior art, since now the deformations are introduced into the optical element via the bearing feet themselves, and it is consequently possible to dispense with uniform fastening of the optical elements to an inner ring of a

mount transferring the deformation. In this way, the number of bearing feet (for example 8, 12 or 16), which require comparatively great expenditure for their production and adjustment, is significantly reduced and
5 the resting of the lens, on fewer bearing feet altogether, is improved with regard to the possibility of active, semi-active and passive adjustment.

Furthermore, the arrangement may be formed in such a
10 way that, in a particularly favorable development of this idea, only some of the bearing feet, for example every second one, or bearing feet arranged at an appropriate angle in relation to one another, for example every 90°, are formed as bearing feet that can be
15 manipulated. In this way the expenditure with regard to the actuators can be further reduced, the specific introduction of the deformation through the respective bearing feet themselves having the effect that the possibility of deforming the optical element is nevertheless
20 improved in comparison with the prior art, since a more specific introduction of force takes place.

The adjustment arrangement according to the invention may be provided in an advantageous way in the case of
25 an optical element that is provided in a projection lens system in semiconductor lithography, such as for example a lens.

For precise mounting, in particular low-deformation
30 mounting, along with appropriate elasticity, the bearing feet may be appropriately adapted. For this purpose, they may be formed for example as solid joints, which may be formed for example in a U-shaped manner.

For specific deformation of the optical element, actuators may then engage the bearing feet, for example where they are formed as solid joints.

5 Further advantageous configurations of the invention emerge from the remaining subclaims and the exemplary embodiments, which are explained below on the basis of the drawing, in which:

10 Figure 1 shows a representation of the principle of a construction according to the invention with an actuator indicated in principle;

15 Figures 2a and 2b show possible embodiments of an actuator in a construction according to Figure 1;

Figure 3 shows an alternative embodiment of an
20 actuator in a construction according to Figure 1;

Figure 4 shows an alternative possibility for
25 the configuration of a bearing foot;

Figure 5 shows a further alternative embodiment of the configuration of a bearing foot;

30 Figure 6 shows an enlarged representation of the region VI from Figure 5;

Figure 7 shows a representation of the principle of a possible arrangement of manipulable bearing feet and fixed bearing feet;

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Figure 8 shows an alternative possibility for arranging manipulable bearing feet and fixed bearing feet;

10 Figure 9 shows a further alternative possibility for arranging manipulable bearing feet and fixed bearing feet; and

Figure 10 shows a projection exposure machine with a projection lens system.

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Figure 1 shows an optical element 1, here a lens, which is mounted in a mount 3 by means of bearing feet 2. The bearing feet 2 are formed in an approximately L-shaped manner and are connected at their one leg 2a to the mount 3. At the free end of their other leg 2b, they have a bearing surface 4 for the optical element 1.

25 The bearing feet 2 are made with a comparatively small wall thickness, so that they have a certain intrinsic elasticity, which permits mounting of the optical element 1 in the mount 3 that is as ideal as possible and initially without any deformation, it being possible
30 for the component referred to here as the mount 3 also to represent merely an inner ring of a mount that can be manipulated with respect to an outer ring.

The optical element 1 thus initially mounted without any deformation is then to be deformed in a way corresponding to the requirements of the optical system, in particular a lens system for semiconductor lithography, which is not represented in its entirety. For example, it may be meaningful to impress an astigmatism on the optical element 1. For this purpose, actuators 5, which are indicated in principle here by an arrow, are provided at least in the case of some of the bearing feet 2.

The actuator 5 is arranged in the region of a holding element 6, which is firmly connected to the mount 3, and in this way acts on the leg 2b of the bearing foot 2 having the bearing surface 4.

The arrow symbolizing the actuator 5 in this case points in both directions, although one direction is undoubtedly generally adequate for the action of the force, depending on the type of actuator 5, since the other direction of the force is realized by the force of gravity exerted by the optical element 1.

If all, or at least some, of the bearing feet 2 are then provided with such an actuator 5, the optical element 1 can be manipulated or deformed in this region by the respective actuator 5 in a direction orthogonal to the circumference which is mostly the direction of the optical axis 7, which in optics is generally referred to as the z direction.

In principle, it would undoubtedly be desirable here to achieve exclusive deformation of the optical element 1,

without the optical element 1 thereby being changed in its position with regard to the optical axis 7, that is to say manipulated, by appropriate exposure of the individual bearing feet 2 to the appropriate forces. The possibility of providing the respective bearing feet 2 with the respective actuator 5 and in this way being able to introduce an appropriate direction of force virtually in every region of the optical element 1 allows such a meaningful deformation of the optical element 1 to be achieved.

Figure 2a then shows an actual exemplary embodiment of one of the actuators 5, as already mentioned above in principle.

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The actuator 5 is in this case configured as a pneumatic or hydraulic actuator 5a, that is to say is actuated by means of a pressure p . Here, too, the force of the weight exerted by the optical element 1 again acts as the restoring force.

The introduction of the force into the optical element 1 takes place by changing the pressure p , which is directed via a feed line 8 in the holding element 6 to a bellows 9 arranged between the holding element 6 and the one leg 2b of the bearing foot 2. Depending on the pressure p introduced, appropriate manipulation of the respective bearing foot 2 is obtained with the actuator 5a, and this in turn then brings about a deformation of the optical element 1 in precisely the region in which the bearing foot 2 is arranged.

Figure 3 shows a further possibility for the configuration of the actuator 5.

The actuator 5 in the exemplary embodiment represented in Figure 3 comprises an actuating screw 10, which acts on the leg 2b of the bearing foot 2 via a spring element 11. Here, too, the restoring force, against the force of the spring, is in turn applied by the force of the weight of the optical element 1.

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In principle, it would in this case be possible in the exemplary embodiment represented here to configure the actuator 5 merely as an adjusting element, that is to say to use the actuating screw 10 for passive adjustment. As an alternative to this, it would of course also be possible here to provide the actuating screw 10 with an appropriate drive, for example a motor drive, in order to permit a semi-active possibility of adjustment in the form of an actuator during the operation of the optical system.

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Figure 4 then shows another embodiment of the bearing foot 2. The bearing foot 2 is formed here in one piece with the mount 3, which is also possible in principle in the case of the exemplary embodiments already mentioned above, but is not necessary there.

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Here, the bearing foot 2 comprises a lever element 2c, which is connected by means of two solid joints 12 on one side to the mount 3 and on the other side to a part 2d of the bearing foot 2 that carries the bearing surface 4.

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Since the solid joints 12 are spaced apart from each other by the width of the lever element 2c, there is the possibility of realizing a displacement of the part 2d, and consequently of the bearing surface 4, in the direction of the optical axis 7 when there is a deflection of the lever element 2c in a direction perpendicular to the optical axis 7.

In the exemplary embodiment represented in Figure 4, this is achieved by an actuating screw 10 as the actuator 5, which engages on the side of the lever element 2c remote from the solid joints 12. The movement of the lever element 2c can be achieved by means of the actuating screw 10. This movement of the lever element 2c is thereby transferred in a monitored manner by the fastening of the lever element 2c by means of the solid joints 12 to the part 2d of the bearing feet 2 that is carrying the bearing surface 4, and consequently brings about the introduction of a force into the optical element 1 that at least runs onto the optical element 1 at least approximately in the direction of the optical axis 7. The actuating screw 10 may in this case of course again engage the lever element 2c by means of a spring element 11, which is not represented here however, or be designed as a pneumatic or hydraulic actuator.

In principle, it would of course also be conceivable and meaningful to configure all the actuators 5 of the exemplary embodiments presented so far and those still to be described later in some other form, for example as active actuators, for example by piezo elements or piezo stacks, and in this way produce specific deforma-

tions of the lens 1 during the operation of a lens system in which the lens 1 is installed, whereby the path of rays in the lens system can be correspondingly influenced.

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Figure 2b shows as an example a piezo stack 15, which takes the place of the hydraulic or pneumatic actuator 5a according to Figure 2a.

10 As in the case of the exemplary embodiment described previously in Figure 3, here, too, it is also possible for the actuating screw 10 in turn to be actuated actively as an actuator by means of a motor drive or the like, so that, apart from a purely passive adjustment,
15 a semi-active readjustment of settling effects can also be performed during the operating period and, if appropriate, active control of the deformation of the optical element 1 can also be performed during actual operation.

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As also already in the case of the exemplary embodiments described above, the force of the weight of the optical element 1 acts here as the restoring force, so that it is ensured by the force of the weight that the
25 lever element 2c is always pressed against its actuator 5, so that a direct manipulation of the lever element 2c is possible.

Figure 5 then shows a further embodiment of the bearing
30 foot 2, which in principle corresponds to the construction just described in Figure 4 with the lever element 2c. However, the bearing foot 2 is in this case formed in a U-shaped manner, one leg 2e of the U-shaped bear-

ing foot 2 being connected to the mount 3. This connection may either be realized again as a one-piece configuration of the bearing foot 2 with the mount 3 or it is also conceivable that, as represented here, the bearing foot 2 is connected to the mount 3 by means of appropriate connecting techniques, such as welding, adhesive bonding, screwing or the like.

The other leg 2f of the bearing foot 2 that is formed in a U-shaped manner carries on its side remote from a base element 2e the part of the bearing foot 2 that is designated by 2d and is connected to the optical element 1 via the bearing surface 4. To create a defined movement of the part 2d of the bearing foot 2 for the operation still to be explained in detail below, the at least one solid joint 12 is arranged between the part 2d and the leg 2f of the bearing foot 2.

By means of an actuating screw 10, which together with a motor drive 13 indicated in principle here, for example an electric motor, forms the actuator 5 in the form of an actuator 5a, the region of the base 2g of the bearing foot 2 can be displaced in a direction at least approximately perpendicular to the optical axis 7. The construction of the bearing foot 2 in its U-shaped configuration, which may also be regarded as a slotted lever, then brings about the effect of a manipulation of the part 2d of the bearing foot 2 against the force of the weight of the optical element 1.

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The possibilities arising from this manipulation are the same as those already described above.

The construction described in Figure 5 shows the possibility in this case, however, that it permits by its configuration an ideal possibility for introducing a stepping-up or stepping-down transmission movement of the actuator 5a onto the movement of the bearing surface 4. At the same time, this produces a comparatively soft construction which, when the actuator 5a is not operated, permits mounting of the optical element 1 in its starting position at least approximately without any deformation.

In order then to avoid any displacement of the optical element 1 in its plane perpendicular to the optical axis 7, the bearing foot 2 represented in Figure 5 also has a stabilizing element 14, which is formed in the manner of a membrane or the like, so that in practice it does not impair the movement of the bearing foot 2 or of the bearing surface 4 in the direction of the optical axis 7, but effectively prevents the movement in the plane perpendicular thereto.

The stabilizing element 14 is represented once again in a detailed form in Figure 6. The thickness of the stabilizing element 14 is made comparatively thin in comparison with the thicknesses of the two legs 2f, 2e of the bearing foot 2 and the stabilizing element 14 is connected to the respective legs of the bearing foot 2 via two solid joints 12.

This achieves the effect that a movement in the direction of the optical axis 7 can take place at least approximately unhindered, while a deflection of the opti-

cal element 1 in a plane perpendicular to the optical axis 7 is effectively prevented.

Figures 7, 8 and 9 show various possibilities for ar-
5 ranging such bearing feet 2 that can be manipulated by means of an actuator 5 on their own or together with fixed bearing feet that are not provided with an actuator 5.

10 The fact that a deformation applied to the inner ring of the mount now no longer has to be introduced as uniformly as possible into the optical element 1, as in the case of the prior art, but that the bearing foot 2 itself can be manipulated in order to deform the opti-
15 cal element 1 in a specific way, means that far fewer bearing feet 2 than in the case of the prior art are now required.

In the exemplary embodiments represented here, six of
20 the bearing feet 2 are respectively represented. The bearing feet identified by the cross are intended in this case to be the bearing feet 2 that have the appropriate actuator 5 or actuators 5a and consequently permit the possibility of introducing a deformation into
25 the optical element 1 through a force acting in the direction of the optical axis 7.

The construction according to Figure 7 allows three-wave (three-leaf clover) deformations of the optical
30 element 1 to be applied, while the construction according to Figure 8 permits the introduction of an astigmatism in one plane.

Figure 9 shows the most variable construction, which however also involves the greatest expenditure with regard to the control of the actuators 5 or actuators 5a on account of the costs arising in production. In this
5 construction, a number of deformations can be introduced into the optical element 1 and then be superposed in the latter to form the corresponding wave aberrations.

10 It would of course be quite conceivable also to realize a far greater number of fixed and/or manipulable bearing feet 2', 2, for example twelve or sixteen manipulable bearing feet allowing a multiplicity of wave aberrations to be produced in the optical element. In
15 particular, however, it is meaningful if astigmatic and three-wave distortions can be introduced, which can be ideally realized for example in an arrangement with eight or twelve bearing feet. Higher-order wave aberrations are often of secondary importance for the qual-
20 ity of the optical imaging quality to be achieved. The expenditure in terms of costs and components could only be justified with difficulty from an economic viewpoint.

25 In Figure 10, a projection exposure machine 16 for microlithography is represented in principle. This serves for exposing patterns on a substrate which is coated with photosensitive materials, generally consists predominantly of silicon and is referred to as a
30 wafer 17, for the production of semiconductor arrangements, such as for example computer chips.

The projection exposure machine 16 in this case substantially comprises an exposure arrangement 18, a arrangement 19 for receiving and exactly positioning a mask provided with a grid-like pattern, the so-called
5 reticle 20, by which the later patterns on the wafer 17 are determined, a arrangement 21 for securing, moving and exactly positioning this very wafer 17 and an imaging arrangement, to be specific a projection lens system 22 with a number of optical elements, such as for
10 example lenses 1, which are mounted in a lens-system housing 23 of the projection lens system 22 by means of mounts 3.

The basic functional principle in this case provides
15 that the patterns introduced into the reticle 20 are exposed onto the wafer 17 with a reduction in the size of the patterns.

Once exposure has taken place, the wafer 17 is moved
20 further in the direction of the arrow, so that a multiplicity of individual zones, each with the pattern predetermined by the reticle 20, are exposed on the same wafer 17. On account of the step-by-step advancing movement of the wafer 17 in the projection exposure machine 16, the latter is also often referred to as a
25 stepper.

The exposure arrangement 18 provides a projection beam
24, for example light or similar electromagnetic radiation, required for projecting the image of the reticle
30 20 onto the wafer 17. A laser or the like may be used as the source for this radiation. The radiation is shaped in the exposure arrangement 18 by means of opti-

cal elements in such a way that, when it impinges on the reticle 20, the projection beam 24 has the desired properties with regard to diameter, polarization, shape of the wave front and the like.

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An image of the reticle 20 is produced by means of the projection beam 24 and transferred by the projection lens system 22 in an appropriately reduced size onto the wafer 17, as already explained above. The projection lens system 22 has a multiplicity of individual refractive and/or diffractive optical elements, such as for example lenses 1, mirrors, prisms, end plates and the like. In this case, one or more lenses 1 may be mounted in the way represented in Figures 1-9 and described above and adjusted or deformed in order to optimize the path of rays.

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